

7 family members for:

EP0040670

Derived from 5 applications.

- 1** **POROUS VINYLIDENE FLUORIDE POLYMER MEMBRANE AND PROCESS FOR ITS PREPARATION**
Publication info: **CA1170010 A1** - 1984-07-03
- 2** **Porous vinylidene fluoride polymer membrane and process for its preparation.**
Publication info: **DE3172472D D1** - 1985-11-07
- 3** **Porous vinylidene fluoride polymer membrane and process for its preparation.**
Publication info: **EP0040670 A2** - 1981-12-02
 EP0040670 A3 - 1982-02-10
 EP0040670 B1 - 1985-10-02
- 4** **POROUS VINYLIDENE FLUORIDE POLYMER MEMBRANE AND MANUFACTURE THEREOF**
Publication info: **JP56152851 A** - 1981-11-26
- 5** **Porous vinylidene fluoride polymer membrane and process for its preparation**
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⑥④ **Porous vinylidene fluoride polymer membrane and process for its preparation.**

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US-A-3 642 668
US-A-3 817 772</p> | <p>⑦① Proprietor: PENNWALT CORPORATION
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Description

The invention is directed to a process for preparing an ultrafiltration membrane of a resinous, film-forming polymer selected from the group consisting of (a) vinylidene fluoride homopolymer, (b) copolymers of at least 70 weight percent of vinylidene fluoride and up to 30 weight percent tri- or tetra-fluoroethylene, and (c) a blend of no less than about 75 weight percent of either (a) or (b) with no greater than about 25 percent of a thermoplastic methyl methacrylate polymer, said membrane having a surface layer containing a multiplicity of pores having a diameter within the range of from 1 to 100 nm, and a support layer thicker than and having less resistance to fluid flow than said surface layer, by casting from solvent/non-solvent systems.

Methods for preparing membranes containing pores of dimensions useful for filtering out substances of various sizes, including salts in solution and viruses are known. However, none of these disclosed methods has been found to be satisfactory for preparing membranes of vinylidene fluoride polymer having a pore size range suitable for ultrafiltration. Furthermore, known solvent casting methods of forming porous vinylidene fluoride polymer sheets require that the sheets be held under restraint during the forming process to avoid uneven shrinkage causing a wrinkled, rough-surfaced product.

Methods for preparing porous membranes and the resulting products are disclosed in a number of publications. US—A—3 133 132 describes cellulose ester membranes prepared from solutions containing pore-forming perchlorate salts. This document does not teach one how to make vinylidene fluoride polymer membranes having ultrafiltration characteristics. US—A—3 567 810 also describes methods for preparing membranes, however, vinylidene fluoride polymer membranes are not described in this document. US—A—3 607 329 describes methods of preparation for membranes of cellulose acetate butyrate. The disclosure of this document does not suggest that the method of preparation is useful for preparing membranes of any other polymer. US—A—3 817 772 discloses porous polymer membranes, including polyvinylidene fluoride membranes. In the production of these polymer membranes, the pores are formed by lixiviation of the film to remove inorganic salt from the binder (polymer) matrix. The production of asymmetric membranes as intended according to the present invention is not disclosed in this document. According to US—A—3 948 823 cross-linked (nonthermoplastic) copolymers are used to form membranes which resist the force of high hydraulic pressure during filtration. The method of forming porous membranes involves forming a solution of the matrix polymer (which may be polyvinylidene fluoride) an ADD polymer (for control of porosity) a crosslinking agent, a solvent for the matrix polymer and a solvent for the ADD polymer. Asymmetric membranes as intended in accordance with the present invention are not disclosed. US—A—4 069 151 describes the preparation of polyether-polycarbonate block polymer membranes from an organic solvent solution of the block polymer dissolved in a suitable solvent for this material. There is no suggestion that the method of this document would be useful for preparation of vinylidene fluoride polymer membranes.

Japanese patent 49—126 572 discloses the use of a combination of slow-drying and fast-drying solvents to prepare a polyvinylidene fluoride membrane having very fine pores. DE—A—2 735 443 describes a process of forming membranes from graft copolymers wherein polyvinylidene fluoride is used as a base polymer. Moreover, FR—A—2 333 825 and US—A—3 615 024 disclose processes for casting PVDF membranes from solvent/non-solvent systems. FR—A—2 333 825 also mentions TFE copolymers. US—A—3 642 668 mentions higher-boiling alcohols as suitable non-solvents although this document is concerned with two-stage processes.

Particularly US—3 615 024 discloses a process for making a porous polymer membrane by casting a solvent-diluent dope of the polymer on a surface, leveling the membrane for about a minute, thereafter washing preferentially one surface of the membrane with a diluent liquid such as water or methyl alcohol, and then replacing all of the solvent with the diluent. Polyvinylidene fluoride is mentioned as a polymer from which membranes may be prepared in accordance with the disclosure although there is no specific working example of its use. Solvents such as dimethyl formamide, dimethyl acetamide, dimethyl sulfoxide and N-methyl pyrrolidone are disclosed as suitable solvents for certain polymers used in the working examples. The product of this known process is disclosed to be an asymmetric membrane having a thin porous layer or "skin" having pores ranging in size of from 1.0 to 1000 nm. The skin is supported on a much thicker layer through which fluid can pass with little hydraulic resistance.

The disadvantages of these prior art processes are described in US—A—3 615 024, column 11, lines 50 to 56 and FR—A—2 333 825 at page 2, lines 28 to 30. US—A—3 642 668 does not disclose an ultrafiltration membrane since the pore sizes of this reference range from 0.5 to 2 μ m.

The object of the present invention is to overcome the disadvantages of the prior art processes by selecting specific compositions and process conditions from the broad range of the state of the art in order to improve the characteristics of PVDF membranes.

According to the present invention this object is achieved in a process as defined above by casting on a smooth solid surface a solution of said resinous, film-forming polymer having a polymer concentration ranging from 12 to 32 weight percent, 65 to 80 weight percent of a solvent selected from the group consisting of triethyl phosphate, hexamethyl phosphoramide, 1-methyl-2-pyrrolidinone, dimethyl acetamide, dimethyl formamide, propylene carbonate and mixtures of said solvents, and from 1 to 10 weight percent of a non-solvent for said polymer selected from the group consisting of glycerol, ethylene

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used. Alternatively, a water-wet, gel membrane may be used provided the water is removed by exchange with suitable water miscible exchange liquid.

Membranes prepared with blends of vinylidene fluoride polymer and methyl methacrylate polymer may be beneficially extracted after gelation with acetone or similar solvent to selectively dissolve some of the methacrylate polymer. This treatment is not critical for the preparation of ultrafiltration membranes but appears to increase permeability somewhat. The extraction step is carried out, for example, by immersing the porous membrane in the solvent overnight at room temperature and then thoroughly washing the membrane with distilled water.

The resinous, thermoplastic methyl methacrylate polymer which is useful for this invention is a methyl methacrylate homopolymer or a copolymer of at least a major proportion of methyl methacrylate and at least one other copolymerizable monomer including, for example, lower alkyl methacrylates, styrene, alpha methylstyrene and acrylonitrile. The methacrylate polymer is used in the blend in amounts of no greater than about 25 percent, based on the weight of the blend. The vinylidene fluoride polymer component of the blend is either the homopolymer or a copolymer of at least 70 weight percent vinylidene fluoride with tri- or tetrafluoroethylene.

The method of preparing the resinous, thermoplastic vinylidene fluoride and methacrylate polymers is not critical to the process described herein. Emulsion polymerization or suspension polymerization techniques are usually employed.

Blends or alloys of vinylidene fluoride resins and methacrylate resins are prepared by mixing the resins in one of the solvents, e.g., triethyl phosphate and non-solvent liquids listed above in a manner as described for the vinylidene fluoride polymer alone. After gelation of the formed alloy membrane, extraction with acetone may be advantageous to increase permeability.

The porous membranes formed by the process of this invention are successfully and advantageously employed in a pressure activated process for separating components of a solution containing solutes of molecular weight above about 6000. These membranes are especially useful in the ultrafiltration of solutions of thermally-unstable or biologically-active materials since this process for separation does not require heat or exposure to chemical reagents. Furthermore, if the materials to be separated are corrosive or hot, the membranes of this invention can be advantageously employed because they are stable up to about 150°C and are resistant to many chemicals.

The preparation of porous membranes in accordance with the process of this invention and their usefulness as ultrafiltration membranes is demonstrated by the following examples.

Example 1

A casting solution was prepared by agitating a mixture of vinylidene fluoride homopolymer powder, (Kynar (trade mark) emulsion grade resin 301) (80 g), glycerol (20 g), and triethyl phosphate (300 g) in a suction flask immersed in an oil bath at 90—100°C for 4 hours. Agitation was provided by a Teflon®-bladed mechanical stirrer. The stirrer was then removed, and the resulting solution was degassed by partial evacuation (266—399 mbar) until all bubbles had disappeared. The solution was free of visible gel particles and was clear. The concentration of glycerol in the solution was 5% by weight.

About 100 ml. of the above solution were cast on a smooth, glass plate (30.5×30.5×0.64 cm previously cleaned with chromic acid, water, and acetone) with a Gardner knife set at 1016 µm (0.10 cm gate). Relative humidity above the casting surface was 65%. After 5 minutes, during which time a portion of the solvent-non solvent had evaporated, the plate and cast film were immersed in a gelation bath, consisting of a mixture of about 10 liters of tap water and ice, for 30 minutes. The membrane formed and floated free of the glass during this time. It was then placed in a bath of warm tap water (50°C) for 5 minutes. The membrane then was stored in distilled water at ambient temperature. At no time during the above steps of forming the membrane was it held or fastened to restrain it from shrinking unevenly. The membrane formed by this process was smooth and unwrinkled.

The above produced membrane was evaluated in a Thin-Channel Ultrafiltration System, using water, Blue Dextran solution, and polyethylene glycol solutions. Data are shown in Table 1.

Examples 2—7

The same general procedure was used as in Example 1 except for the glycerol concentration, which was varied from 1 to 8%. Test results are compared in Table 1.

TABLE 1

Example	Glycerol conc'n. (%)	Feed*	Retention (%)	Flux ** (ml/cm ² /min.)
2	3	BD	≥98	0.01
		H ₂ O	—	0.01—0.02
		C-20	>98	0.01
		C-6	>95	0.01—0.02
		C-1	20—35	0.02
1	5	BD	≥98	0.02—0.08
		H ₂ O	—	0.04—0.1
		C-20	≥98	0.01—0.03
		C-6	70—90	0.03—0.05
		C-1	4—30	0.04—0.05
3	6	BD	≥98	0.06—0.1
		H ₂ O	—	0.1—0.2
		C-20	82—89	0.02—0.04
4	7	BD	≥98	0.2
		H ₂ O	—	0.3—0.5
		C-20	68—79	0.05—0.06
		C-6	0	0.3—0.5
5	8	BD	90	0.05—0.1
		H ₂ O	—	0.3—0.6
		C-20	70—78	0.02—0.05
6	2	H ₂ O	—	0.005—0.007
		C-1	51—76	0.005
		H ₂ O	—	0.005
		C-6	64—92	0.003
		BD	>98	0.004
7	1	H ₂ O	—	<0.001

*BD=0.1% Aqueous Blue Dextran 2000 Solution (M.W. 2,000,000)

C-20=1% Aqueous polyethylene glycol 20M solution (M.W. 15,000—20,000)

C-6=1% Aqueous polyethylene glycol 6000 solution (M.W. 6000)

C-1=1% Aqueous polyethylene glycol 1000 solution (M.W. 1000)

** Flux and retention at 3.1 bar. For Example 6 and 7, flux and retention at 11.5 bar.

45 Examples 8—12

The same general procedure was used as in Example 1 except for the solvent employed. Test results are compared in Table 2.

TABLE 2

Example	Solvent	Blue dextran(*) Flux	Retention	H ₂ O Flux(**)	Polyethylene glycol 20M (***) Flux	Retention
8	Hexamethyl Phosphoramide	0.08—0.09	>98%	0.1		
1	Triethyl Phosphate	0.02—0.08	>98%	0.04—0.1	0.01—0.03	≥98%
9	1-Methyl-2-Pyrrolidinone	0.03	>98%	0.1		
10	Dimethyl Acetamide	0.02—0.03	>98%	0.05		
11	Dimethyl Formamide	0.006	>98%	0.01	0.004	98%
12	Propylene Carbonate	0.1	80—85%	0.25		

* 0.1% Blue Dextran 2000 aqueous solution feed.

Flux in ml/cm²/min. at 3.1 bar.

** Water flux in ml/cm²/min. at 3.1 bar.

*** 1% aqueous solution of polyethylene glycol 20M feed.
Flux in ml/cm²/min. at 3.1 bar.

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Examples 13—20

A comparison of some other non-solvents in the casting solution is set forth in the following table.

5	Example ^(*)	Non-solvent	TABLE 3			Flux
			Feed	Pressure	Retention	
10	13	Glycerol	BD	3.1 bar	>98%	0.02—0.08 ml/cm ² /min.
			H ₂ O	"	—	0.04—0.1
			C-20	"	≥98	0.01—0.03
15	14	Phosphoric Acid	BD	"	>98	0.06—0.07
			H ₂ O	"	—	0.1
			C-20	"	>98	0.03—0.04
20	15	Ethylene Glycol	BD	"	≥95	0.01
			H ₂ O	"	—	0.01
			C-20	"	>98	0.005—0.008
25	16 (Comparative Example)	Pentaerythritol	BD	"	>98	0.001
			H ₂ O	"	—	0.001
			H ₂ O	7.9 bar	—	0.04
			H ₂ O	9.6 bar	—	0.07
30	17 (Comparative Example)	Citric Acid	BD	3.1 bar	>98	<0.001
			H ₂ O	3.1 bar	—	<0.001
			H ₂ O	9.6 bar	—	<0.001
35	18 (Comparative Example)	Bis-Phenol A	H ₂ O	3.1 bar	—	<0.001
			H ₂ O	9.6 bar	—	<0.001
40	19 (Comparative Example)	Acetic Acid	H ₂ O	3.1 bar	—	<0.001
			H ₂ O	3.1 bar	—	<0.001
45	20 (Comparative Example)	Ethyl Acetoacetate	H ₂ O	7.9 bar	—	<0.001
			H ₂ O	7.9 bar	—	<0.001

* Membranes were made with 20% vinylidene fluoride homopolymer, 5% non-solvent, and 75% triethyl phosphate in the casting solution. Other conditions are described in Example 1.

Example 21—23

Vinylidene fluoride—tetrafluoroethylene copolymer resins having the monomer weight percentages reported in the table below were cast as generally described for Example 1 except that solution concentrations were at either 20 or 30 weight percent as reported below and heat stabilization of the membrane was omitted. The ultrafiltration data for these membranes is given in the following table.

TABLE 4								
50	Example	Composition VF ₂ /TFE	Casting solution, conc'n.		Test feed	Membrane evaluation		Pressure
			Polymer	Glycerol		Retention	Flux	
						%	(ml/cm ² /min)	(bar)
55	21	95/5	20%	5%	H ₂ O	—	0.02—0.07	3.1 ↓
					BD	>98	0.004—0.015	
					H ₂ O	—	0.008—0.02	
					C-20M	99	0.003—0.008	
					H ₂ O	—	0.007—0.03	
60	22	70/30	20%	5%	Poor Quality, Not Tested			
	23	70/30	30%	5%	H ₂ O	—	0.001	3.1
65					H ₂ O	—	0.002—0.003	11.5

Examples 24—26

A 20 weight percent solution of a mixture of resins consisting of 16 parts vinylidene fluoride homopolymer and 4 parts of poly(methyl methacrylate) (Lucite 140 (trade mark)) in triethyl phosphate and containing 5 weight percent glycerol, was prepared in a manner similar to the solution preparation in Example 1. Three 1016 μm films of the solution were cast on a glass plate, the solutions allowed to evaporate at room temperature for 5 minutes and the films gelled by immersion in an ice-water bath for 30 minutes. The membranes were then stabilized by immersion in hot water (50°C) for 5 minutes. The resulting membranes were kept wet with water, and flux and water retention properties determined at 3.1 bar by the procedure used in the foregoing examples. The results are shown in the following table.

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Example	Water flux	Blue dextran		Water		C-20 Retention
		Flux	Retention	Flux	Flux	
24	0.16	0.03	>98	0.06	0.02	94
25	0.10	0.03	>98	0.03	0.05	34
26	0.11	0.03	>98	0.06	0.02	94

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Example 27

To demonstrate that vinylidene fluoride polymers produced by a suspension polymerization process are also useful for this invention, a casting solution was prepared by agitating a mixture of vinylidene fluoride homopolymer (Kynar (trade mark) grade 821, suspension grade resin), (60 g), glycerol (24 g), and triethyl phosphate (316 g) for 4 hr at 90—95°C. Agitation was provided by a Teflon®-bladed mechanical stirrer. The stirrer was then removed, and the resulting solution was degassed by partial evacuation (333—532 mbar) until all bubbles had disappeared. The solution was free of visible gel particles and was clear. The concentration of glycerol in the solution was 6% by weight.

A membrane was cast with this solution onto a clean, smooth glass plate with a Gardner knife set at 508 μm . After an evaporation time of 5 min, the plate and cast film were immersed in a gelation bath of iced water (2—3°C) for 30 min. The membrane formed and floated free of the glass during this time.

During the steps of formation of the membrane through gelation, the membrane was not taped or restrained in any way and, surprisingly provided a smooth, unwrinkled membrane product. Later, the membrane was heat stabilized for 30 min in water at 100°C.

Tests were performed on the membrane of this Example in accordance with the procedure described in Example 1 and the results are shown in the following table.

Example	Glycerol conc'n %	Feed	Retention, %	Flux
27	6	B.D.	>98	0.1
		H ₂ O	—	0.07
		C-20	97	0.03

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Example 28

A casting solution was prepared by agitating a mixture of vinylidene fluoride homopolymer powder (120 g), glycerol (36 g), and triethyl phosphate (444 g.) for 1-1/2 hr. at 90—95°C. Agitation was then stopped, the mixture was allowed to cool to room temperature, and was stored overnight in a stoppered container. The following day the mixture was reheated to 90—95°C and agitated for an additional 1-1/2 hr. Agitation was provided by a Teflon-bladed mechanical stirrer. The stirrer was then removed, and the resulting solution was degassed by partial evacuation (333—532 mbar) until all bubbles had disappeared. The solution was free of visible gel particles and was clear. The concentration of glycerol in the solution was 6% by weight.

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Four membranes were cast from this solution onto 30×90 cm (12×36 inch) smooth glass plates. In all cases the temperature of the solution at the time of casting was 91—93°C, the thickness of the cast film was 508 μm , and the relative humidity above the casting surface at the time of casting was 74%. In each case, after the cast film had been allowed to evaporate for 5 min. at ambient temperature, the plate and cast film were immersed in an iced-water gelation bath (2—4°C) for 30 min. The membrane formed and floated free of the glass during this time.

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The membranes were stored in distilled water at ambient temperature for 12 days and then were heat treated by immersion for 30 min. in water at 95—100°C. As soon as the membranes were removed from the hot water they were cooled to ambient temperature by immersion in a large volume of water at ambient temperature.

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The wet membranes were glycerol treated by immersion in glycerol for about 30 min., then were hung vertically by clips attached to one end to allow excess glycerol to drain off. The membranes were then allowed to dry at ambient temperature.

A spiral-wound module was prepared using two of these membranes. It was flushed with water for 30 min. to remove glycerol from the membranes, and then found to retain Blue Dextran quantitatively when tested with a 0.09% aqueous solution of Blue Dextran 2000 at 1.9 bar and ambient temperature.

This module was tested for long term stability at high temperature by operation in an automated ultrafiltration unit for over a month at 85°C. The feed was a 0.4% solution of Elvanol T-25 (trade mark for a fully hydrolyzed polyvinyl alcohol from E.I. DuPont de Nemours & Co.) in deionized water. The feed solution concentration was kept constant by continuously returning the permeate to the feed tank and by adding deionized water as necessary to make up for water lost by evaporation. A pressure of 2.4 bar and a feed recirculation rate of 38 l/min. were used throughout the study.

Representative data is given below.

Time	Flux	Retention of PVA
Start	0.03 ml/cm ² min.	—
2 days	0.02	97.2%
27 days	0.02	97.4%

Example 29

Another batch of membranes was prepared by the same general procedure as in Example 28 except for the following. Solution preparation, requiring a total of 3-1/2 hr., and casting were done on the same day. The glycerol concentration in the casting solution was the same as in Example 28 (6% by weight). The relative humidity during casting was 69%. After gelation in iced-water, the membranes were stored in water for 3 days at ambient temperature, and then were heat treated for 30 min. in water at 95°C. The membranes were then allowed to dry in air at room temperature without prior treatment with glycerol or any other humectant or surfactant.

A spiral-wound module was prepared using two of these membranes. The module was soaked for 1-1/2 hr. in a 1:1 mixture of isopropanol and water and then soaked in pure water overnight. It was flushed with water for about 30 min. to remove any residual alcohol and then found to retain Blue Dextran quantitatively when tested with a 0.09% aqueous solution of Blue Dextran 2000 at 1.9 bar and ambient temperature.

This module was tested for long term stability at high temperature in a 0.4% solution of polyvinyl alcohol by the same procedure and under the same conditions employed in Example 28 except that the pressure was 2.7 bar.

Representative data is given below.

Time	Flux	Retention of PVA
Start	0.03 ml/cm ² min.	93.3%
3 days	0.02	97.3%
7 mo.	0.02	97.5%

Example 30 (comparative example)

A casting solution was prepared by stirring a mixture of polysulfone resin pellets (Udel P-1700, trade mark of Union Carbide Corp.) (75 g) and hexamethyl phosphoramide (425 g) for 5 hrs. at 90—95°C until all of the polymer was dissolved. The solution was then allowed to stand undisturbed for 15 min. at atmospheric pressure to permit air bubbles to escape. The resulting solution was clear and bubble-free.

A 254 µm film of this solution was cast onto a smooth, clean glass plate. Tape had been placed along the edges of the plate prior to casting to assure adherence of the film to the plate during subsequent processing steps. Immediately after the film had been cast the plate and cast film were placed under an electric heater at a temperature of 65.6°C for 3 min. The plate and film were then removed and immersed in a water bath at ambient temperature for gelation. After 30 min. the resulting membrane was cut free of the tape, removed from the glass plate, and stored in water at ambient temperature.

The membrane was tested by the same procedure used for Example 1. Results were as follows:

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	Feed	Retention	Flux
	H ₂ O	—	2.1 ml/cm ² min.
5	B.D.	>98%	0.2
	H ₂ O	—	0.9
	C-20	95%	0.07

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Example 31 (comparative example):

Vinylidene fluoride homopolymer and polysulfone membranes were prepared by procedures illustrated in the foregoing examples.

Membranes were characterized by measuring distilled water flux and the flux and retention of 1% polyethylene glycol 20M solutions at 3.1 bar in a thin-channel ultrafiltration cell.

For chemical stability tests, membrane samples with known flux and retention were soaked in the specified solution or solvent for a given period (usually ~1 month) and then thoroughly rinsed with distilled water and retested. If no significant change in flux or retention was found, the sample was returned to the chemical solution for an additional period.

20 Results are shown in the following tables.

TABLE 7					
	Exposure chemical	Poly(vinylidene fluoride)		Polysulfone	
25	1% NaOCl	6 mo. 8 mo.	OK ¹ failed ²	1 mo.	failed ²
30	10% Na ₂ Cr ₂ O ₇ in 96% H ₂ SO ₄	1 week 1.5 mo.	OK ¹ failed ²	2 hr.	disintegrated
	5% Na ₂ Cr ₂ O ₇ in 48% H ₂ SO ₄	5 mo.	OK ¹	<2 weeks	disintegrated
35	10% H ₂ O ₂	1.5 mo. 5 mo.	OK ¹ failed ²	1 week 1.5 mo.	OK ¹ failed ²
	48% H ₂ SO ₄	25 mo.	OK ¹	5 mo.	OK ¹
40	18% HCl	25 mo.	OK ¹		
	35% HNO ₃	25 mo.	OK ¹	5 mo.	OK ¹
	42% H ₃ PO ₄	25 mo.	OK ¹		
45	10% NaOH	1 mo. 3 mo.	OK ^{1,3} failed ^{2,3}		
50	1% NaOH	24 mo.	OK ^{3,4}		
	1% Na ₂ CO ₃	24 mo.	OK ¹		

55 ¹. No significant change in flux or in retention of polyethylene glycol 20M.

². Became brittle, cracked and chipped.

³. Became discolored.

⁴. Flux has increased and retention of polyethylene glycol has decreased; however, ~90% of the polyethylene glycol still retained.

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TABLE 8

	Exposure chemical	Poly(vinylidene fluoride)		Polysulfone
5	95% Ethanol	5 mo.	OK ¹	5 mo. membrane shrinking ²
	1:1 Acetone/Water	1 mo.	OK ¹	3 weeks membrane shrinking ²
	<i>n</i> -butanol	1 mo.	OK ¹	3 weeks membrane shrinking ²
10	Ethyl acetate	1 mo.	OK ¹	shrivels instantly
	Tetrahydrofuran	1 mo.	OK ¹	dissolves instantly
15	Toluene	1 mo.	OK ¹	shrivels instantly
	Chlorobenzene	1 mo.	OK ¹	dissolves instantly

20 ¹. No significant change in flux or in retention of polyethylene glycol 20M.

². Membrane shrank ~5% and could not be sealed in test cell adequately for testing.

Claims

25 1. A process for preparing an ultrafiltration membrane of a resinous, film-forming polymer selected from the group consisting of (a) vinylidene fluoride homopolymer, (b) copolymers of at least 70 weight percent of vinylidene fluoride and up to 30 weight percent tri- or tetrafluoroethylene, and (c) a blend of no less than about 75 weight percent of either (a) or (b) with no greater than about 25 percent of a thermoplastic methyl methacrylate polymer, said membrane having a surface layer containing a
30 multiplicity of pores having a diameter within the range of from 1 to 100 nm, and a support layer thicker than and having less resistance to fluid flow than said surface layer, by casting from solvent/non-solvent systems, characterized by casting on a smooth solid surface a solution of said resinous, film-forming polymer having a polymer concentration ranging from 12 to 32 weight percent, 65 to 80 weight percent of a solvent selected from the group consisting of triethyl phosphate, hexamethyl phosphoramide, 1-methyl-2-
35 pyrrolidinone, dimethyl acetamide, dimethyl formamide, propylene carbonate and mixtures of said solvents, and from 1 to 10 weight percent of a non-solvent for said polymer selected from the group consisting of glycerol, ethylene glycol, phosphoric acid and mixtures thereof, to form a sheet, evaporating a portion of said liquid mixture from said sheet, and contacting said sheet with a liquid gelation medium.

40 2. The process of claim 1 wherein the resinous, film-forming polymer is vinylidene fluoride homopolymer.

3. The process of claim 1 wherein the resinous, film-forming polymer is a copolymer of at least 70 weight percent of vinylidene fluoride and up to 30 weight percent of tri- or tetrafluoroethylene.

4. The process of claim 2 or 3 wherein the solvent is triethyl phosphate.

5. The process of claim 4 wherein the liquid gelation medium is water.

45 6. The process of claim 1, 2, 4 or 5 wherein, after the membrane is formed, it is subjected to a heat treatment at a temperature ranging up to 100°C.

7. The process of claim 1, 2, 3 or 4 wherein the non-solvent is glycerol.

8. The process of claim 4 wherein the cast sheet is contacted with said liquid gelation medium in the absence of physical restraint on the edges of said sheet.

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Patentansprüche

1. Verfahren zur Herstellung einer Ultrafiltrationsmembran aus einem harzartigen, filmbildenden Polymeren, ausgewählt aus der Gruppe, bestehend aus (a) Vinylidenfluoridhomopolymer, (b)
55 Copolymeren aus mindestens 70 Gew.-% Vinylidenfluorid und bis zu 30 Gew.-% Tri- oder Tetrafluorethylen und (c) einem Gemisch aus nicht weniger als etwa 75 Gew.-% von entweder (a) oder (b) mit nicht mehr als etwa 25% eines thermoplastischen Methylmethacrylatpolymeren, wobei die genannte Membran eine Oberflächenschicht, die eine Vielzahl von Poren mit einem Durchmesser im Bereich von 1 bis 100 µm
60 aufweist als die genannte Oberflächenschicht, besitzt, durch Gießen aus Lösungsmittel-/Nichtlösungsmittelsystemen, dadurch gekennzeichnet, daß man auf eine glatte feste Oberfläche eine Lösung des genannten harzartigen, filmbildenden Polymeren mit einer Polymerkonzentration im Bereich von 12 bis 32 Gew.-%, 65 bis 80 Gew.-% eines Lösungsmittels, ausgewählt aus der Gruppe, bestehend aus Triethylphosphat, Hexamethylphosphoramid, 1-Methyl-2-pyrrolidinon, Dimethylacetamid, Dimethylformamid,
65 Propylencarbonat und Gemischen der genannten Lösungsmittel, und 1 bis 10 Gew.-% eines Nichtlösungsmittels

mittels für das genannte Polymere, ausgewählt aus der Gruppe, bestehend aus Glycerin, Ethylenglykol, Phosphorsäure und Gemischen davon, gießt, um eine Platte zu bilden, einen Teil des genannten Flüssigkeitsgemisches von der genannten Platte abdampft und die genannte Platte mit einem flüssigen Gelierungsmedium kontaktiert.

5 2. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß das harzartige, filmbildende Polymere ein Vinylidenfluoridhomopolymeres ist.

3. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß das harzartige, filmbildende Polymere ein Copolymeres aus mindestens 70 Gew.-% Vinylidenfluorid und bis zu 30 Gew.-% Tri- oder Tetrafluorethylen ist.

10 4. Verfahren nach Anspruch 2 oder 3, dadurch gekennzeichnet, daß das Lösungsmittel Triethylphosphat ist.

5. Verfahren nach Anspruch 4, dadurch gekennzeichnet, daß das flüssige Gelierungsmedium Wasser ist.

6. Verfahren nach Anspruch 1, 2, 4 oder 5, dadurch gekennzeichnet, daß man die Membran nach ihrer 15 Bildung einer Wärmebehandlung bei einer Temperatur von bis zu 100°C unterwirft.

7. Verfahren nach Anspruch 1, 2, 3 oder 4, dadurch gekennzeichnet, daß das Nichtlösungsmittel Glycerin ist.

8. Verfahren nach Anspruch 4, dadurch gekennzeichnet, daß die gegossene Platte mit dem flüssigen Gelierungsmedium in Abwesenheit einer physikalischen Beschränkung auf die Kanten der genannten 20 Platte kontaktiert.

Revendications

1. Procédé en préparation d'une membrane d'ultrafiltration en un polymère résineux filmogène choisi 25 dans le groupe comprenant (a) un homopolymère de fluorure de vinylidène, (b) des copolymères d'au moins 70% en poids de fluorure de vinylidène avec jusqu'à 30% en poids de tri- ou de tétrafluoréthylène et (c) un mélange ne contenant pas moins d'environ 75% en poids de (a) ou (b) avec pas plus d'environ 25% d'un polymère thermoplastique de méthacrylate de méthyle, ladite membrane ayant une couche de surface présentant de très nombreux pores d'un diamètre compris dans l'intervalle de 1 à 100 µm, et une 30 couche de support plus épaisse et moins résistante à l'écoulement d'un fluide que ladite couche de surface, par coulée à partir de systèmes solvant/non-solvant, caractérisé par la coulée sur une surface unie lisse d'une solution dudit polymère filmogène résineux ayant une concentration en polymère de 12 à 32% en poids, contenant 65 à 80% en poids d'un solvant choisi dans le groupe comprenant le phosphate de triéthyle, l'hexaméthylphosphoramide, la 1-méthyl-2-pyrrolidinone, le diméthylacétamide, le 35 diméthylformamide, le carbonate de propylène et des mélanges de ces solvants, et 1 à 10% en poids d'un non-solvant pour ledit polymère, choisi dans le groupe comprenant le glycérol, l'éthylèneglycol, l'acide phosphorique et leurs mélanges, pour former une feuille, l'évaporation d'une portion dudit mélange liquide de ladite feuille et la mise en contact de cette dernière avec un milieu liquide de gélification.

2. Procédé suivant la revendication 1, dans lequel le polymère filmogène résineux est un 40 homopolymère de fluorure de vinylidène.

3. Procédé suivant la revendication 1, dans lequel le polymère filmogène résineux est un copolymère d'au moins 70% en poids de fluorure de vinylidène et d'une proportion allant jusqu'à 30% en poids de tri- ou de tétrafluoréthylène.

4. Procédé suivant la revendication 2 ou 3, dans lequel le solvant est le phosphate de triéthyle.

45 5. Procédé suivant la revendication 4, dans lequel le milieu liquide de gélification est l'eau.

6. Procédé suivant la revendication 1, 2, 4 ou 5, dans lequel, après que la membrane a été formée, elle est soumise à un traitement à la chaleur à une température s'élevant à 100°C.

7. Procédé suivant la revendication 1, 2, 3 ou 4, dans lequel le non-solvant est le glycérol.

8. Procédé suivant la revendication 4, dans lequel la feuille coulée est mise en contact avec ledit milieu 50 liquide de gélification sans entrave physique sur les bords de ladite feuille.

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